

# TENTATIVE TRACT 20348

County of San Bernardino, CA

## DRAINAGE STUDY

April 17, 2020



Reference 900-900.105

PREPARED BY:

**Encompass Associates, Inc.**

5699 Cousins Place  
Rancho Cucamonga, CA 91737

909-684-0093

Fax-909-586-6979

[askers@encompasscivil.com](mailto:askers@encompasscivil.com)

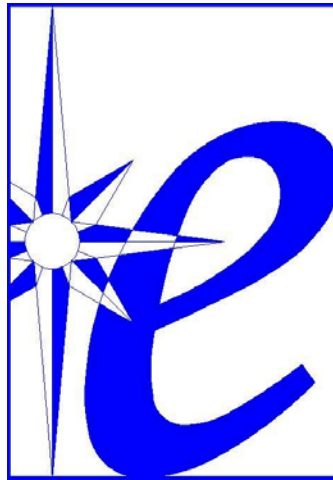
[www.encompasscivil.com](http://www.encompasscivil.com)

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Aaron T. Skeers

Date

R.C.E. 62183 Exp. 9/30/21

[askeers@encompasscivil.com](mailto:askeers@encompasscivil.com)  
[www.encompasscivil.com](http://www.encompasscivil.com)

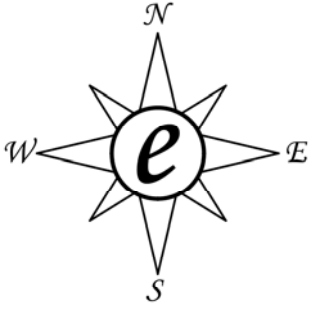
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# VICINITY MAP

SCALE: N.T.S

## ***DISCUSSION***

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The purpose of this drainage study is to determine the drainage facility requirements for Tentative Tract 20348 in County of San Bernardino.

The proposed project is a subdivision of 60 detached condominium units on one lot, on three existing parcels, comprised of vacant land and a mobile home community on a 4.1 acre property at 5611, 5639 and 5681 Mission Boulevard, on the south side between Vernon Avenue and Benson Avenue. A condominium project is under development on the west side, with single-family residences to the south, Benson Avenue to the east, and light industrial across Mission to the north.

In addition to the residential buildings, the condo site will be comprised of drives, parking, a private park with tot lot, and paseos throughout. There will be one DA (DA 1), 179,162 sf, with 45,000 sf pervious and 101,314 sf impervious (66,250 sf buildings, 35,064 sf pavement, sidewalks and driveways).

All runoff drains to Benson Avenue via surface flows. Condominium unit runoff will be collected via area drains inlets and pipes and conveyed to an underground perforated pipe infiltration system. Discharge in excess of the water quality volume will surface drain out to Benson Avenue to the southeast.

The 100-year storm event was modeled in the rational method hydrology calculations in this study. The developed condition does not exceed the existing condition due to the partially developed nature of the existing property, and because proposed runoff will be lengthened and flattened, increasing the time of concentration.

The rational method hydrologic model, as defined by Flood Control for San Bernardino County, was followed in the determination of storm runoff.

# **RATIONAL METHOD**

# **HYDROLOGY**

Rational Method Hydrology Calculations

SWC Mission/benson

Date: 4/11/2020

100 -year storm runoff

Antecedent Moisture Condition Used: AMC III

1-hour point rainfall from Isohyet Map is 1.51 inches per hour.

Slope of Intensity-Duration Curve is 0.6.

0.1 To 0.2 Initial flow through Subarea

Initial Flow through Subarea 1

Upstream Elevation at Node 0.1 is 43 ft.

Downstream Elevation at Node 0.2 is 39 ft.

Flow length is 297 ft.

Land Use	Soil Type	Area (AC)
grass poor	A	2.4
mobile home park	A	1.7

Time of Concentration =  $T_c = K * (\text{length}^3 / \Delta_{EL})^{0.2} = 0.525 * (297^3 / 4)^{0.2} = 12.117$  minutes.

Rainfall Intensity =  $e^{(-\text{Slope} * \text{Log}(\text{desT}) + \text{Log}(\text{refI}) + \text{Slope} * \text{Log}(\text{refT}))}$

$$= e^{(-0.6 * \text{Log}(12.117) + \text{Log}(1.51) + 0.6 * \text{Log}(60))} = 3.943 \text{ in/hr.}$$

Peak Runoff =  $0.9 * (I - A_p * F_p) * \text{Area} = 0.9 * (3.943 - 0.78 * 0.4) * 4.1 = 13.39$  cfs.

Peak Flow (cfs): 13.39 TC (min): 12.12

1 To 1.1 Initial flow through Subarea

Initial Flow through Subarea 3

Upstream Elevation at Node 1 is 42 ft.

Downstream Elevation at Node 1.1 is 40.5 ft.

Flow length is 507 ft.

Land Use	Soil Type	Area (AC)
condominiums	A	1.2

Time of Concentration =  $T_c = K * (\text{length}^3 / \Delta_{EL})^{0.2} = 0.3592 * (507^3 / 1.5)^{0.2} = 13.903$  minutes.

Rainfall Intensity =  $e^{(-\text{Slope} * \text{Log}(\text{desT}) + \text{Log}(\text{refI}) + \text{Slope} * \text{Log}(\text{refT}))}$

$$= e^{(-0.6 * \text{Log}(13.903) + \text{Log}(1.51) + 0.6 * \text{Log}(60))} = 3.631 \text{ in/hr.}$$

Peak Runoff =  $0.9 * (I - A_p * F_p) * \text{Area} = 0.9 * (3.631 - 0.35 * 0.74) * 1.2 = 3.64$  cfs.

Peak Flow (cfs): 3.64 TC (min): 13.9

1.1 To 1.1 Catch Basin Flow Interception

Sump Catch Basin Sizing Calculation at Node 1.1.

User-Defined Sump Depth at Catch Basin = 0.2.

Sump Depth Exceeds 1.4 x Opening Height: using Orifice Formula:

$$Q = C * (\text{OpeningHt} * \text{Length}) * \text{Sqrt}(2 * G * H), 3.64 = 0.6 * (0 * \text{Length}) * \text{SQRT}(2 * 32.2 * 0.2).$$

Partial Flow Interception in 4 ft. inlet is 0 cfs.

Catch Basin Length = 4 ft.

Peak Flow (cfs): 3.64 TC (min): 13.9

1.1 To 1.2 Pipe flow through Subarea

Rational Method Hydrology Calculations

Pipe Flow From Node 1.1 to Node 1.2.

Upstream Elevation at Node 1.1 is 35 ft. Downstream Elevation at Node 1.2 is 34 ft.

Flow length is 146 ft.

Average Pipe Slope =  $(35 - 34) / 146 = 0.007$  ft/ft.

Pipe Diameter =  $((Q * N) / (1.486 * So^{0.5} * 0.31169))^{3/8}$   
 $= ((3.64 * 0.01) / (1.486 * 0.007^{0.5} * 0.31169))^{3/8} = 1.5$  ft.

Flow Depth, Iterate:  $Q = (1.486 / N) * Area * (Area / WetPer)^{2/3} * s^{0.5}$

Try: 0.59 ft., Flow Area =  $Dia^2 / 8 * (Angle - Sin(Angle))$ ,

where Angle =  $2 * Acos(1 - 2 * Depth / Dia) = 2 * Acos(1 - 2 * 0.59 / 1.5) = 2.71$

Flow Area =  $1.5^2 / 8 * (2.71 - Sin(2.71)) = 0.65$  sf.

Pipe Velocity =  $Q / Area = 3.64 / 0.65 = 5.64$  ft/sec.

Pipe Travel Time =  $Length / Velocity = 146 / 5.64 = 25.89$  sec., Mainstream TC = 14.33 minutes.

Peak Flow (cfs):  TC (min):

To  Add Subarea at Node

Add Flow from Subarea 4

Land Use	Soil Type	Area (AC)
condominiums	A	2.9

At Node 1.2: Time of Concentration = 14.33 minutes, Rainfall Intensity = 3.565 in/hr.

Subarea Peak Runoff =  $0.9 * (I - Ap * Fp) * Area = 0.9 * (3.565 - 0.35 * 0.74) * 2.9 = 8.62$  cfs.

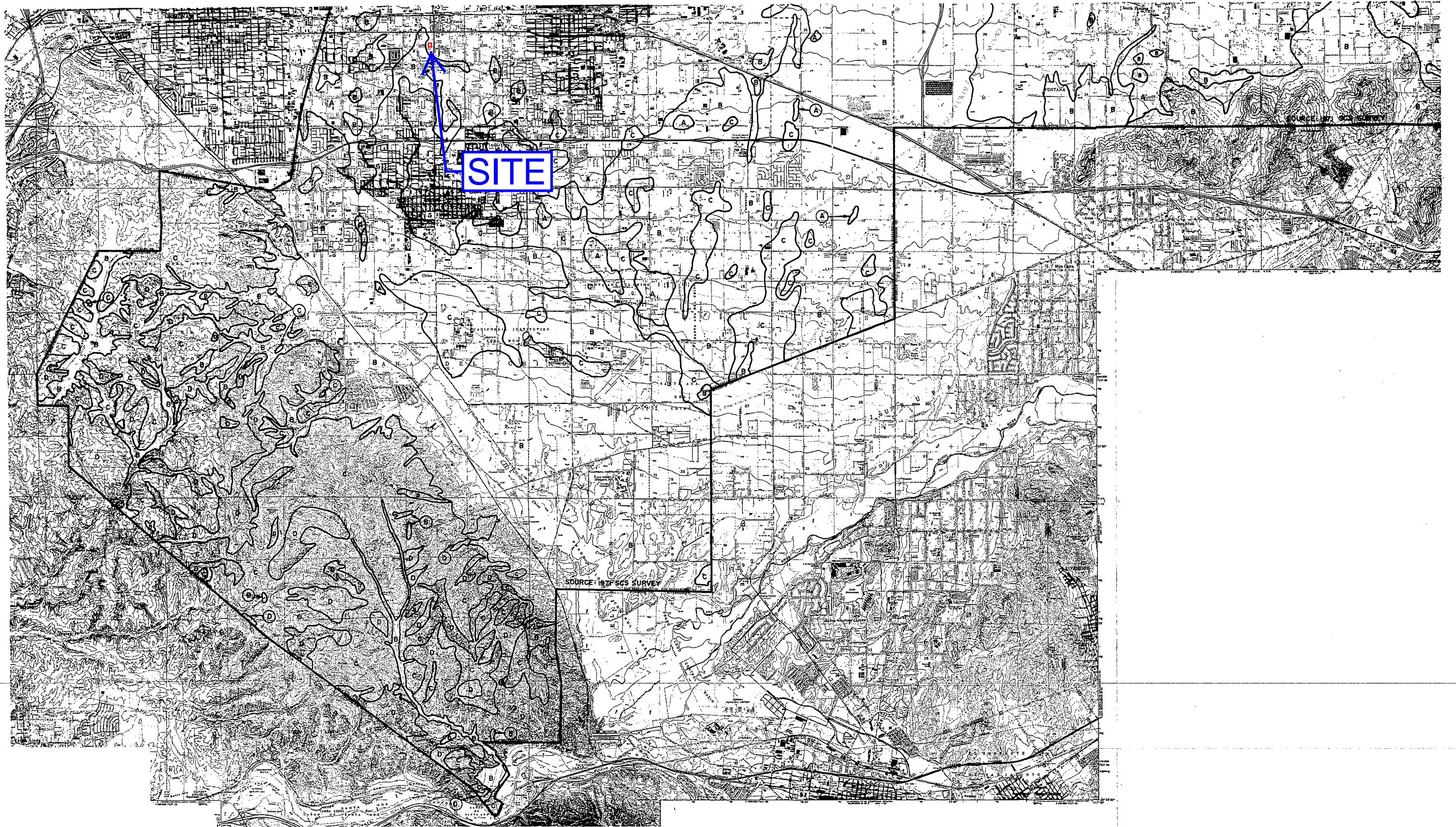
Area-Averaged  $Ap = 0.35$ , Area-Averaged  $Fp = 0.74$  in/hr, Total Area = 4.1 ac, Effective Area = 4.1 ac

Total Peak Runoff =  $0.9 * (I - Ap * Fp) * Area = 0.9 * (3.565 - 0.35 * 0.74) * 4.1 = 12.18$  cfs.

Peak Flow (cfs):  TC (min):

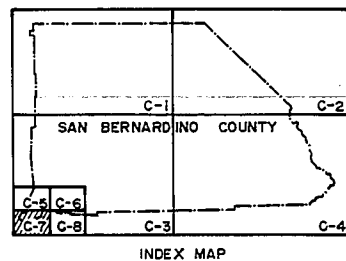


## **REFERENCES & MAPS**



**SITE**

SOURCE: 1977 SGS SURVEY



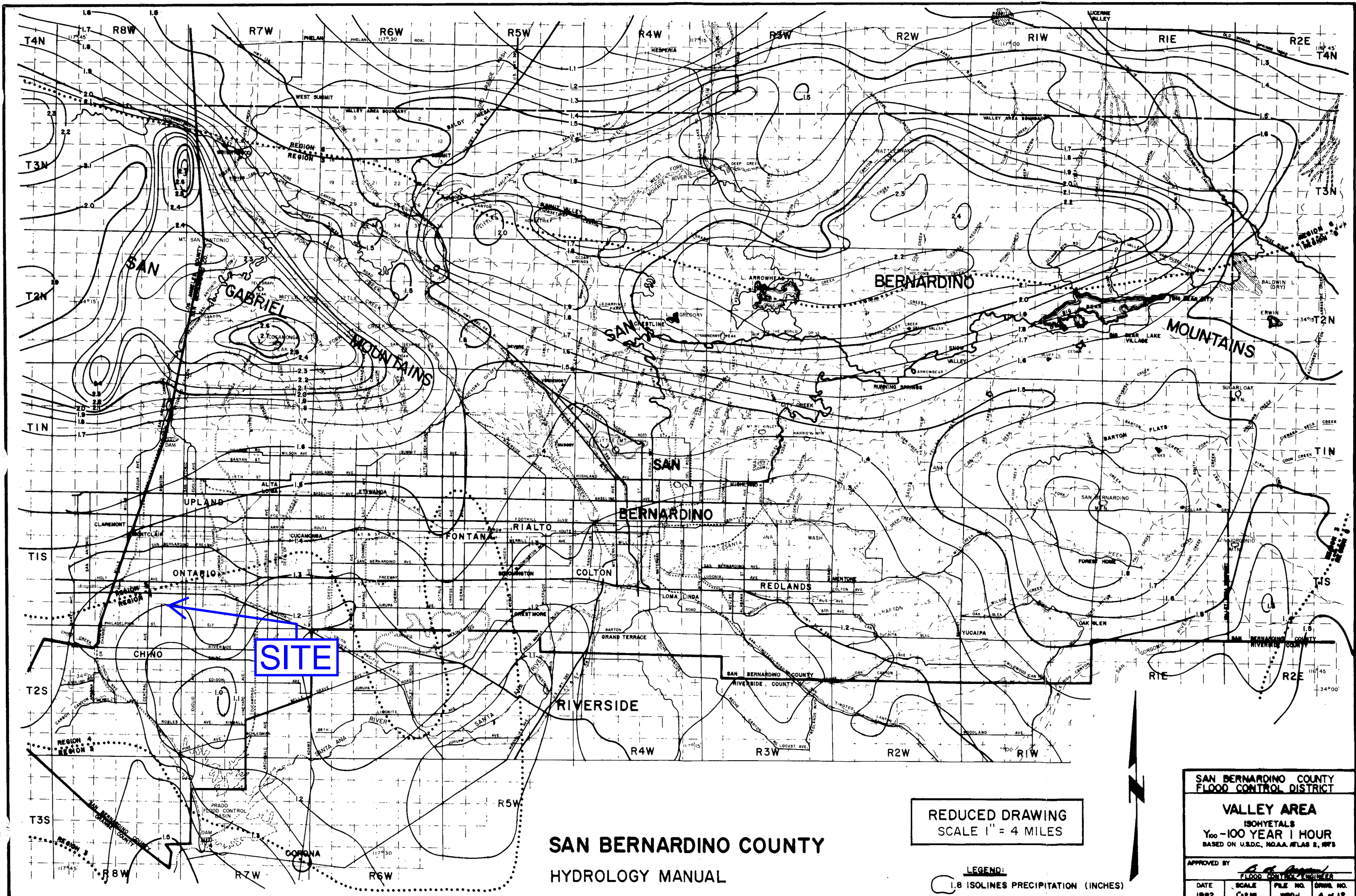
- LEGEND
- SOIL GROUP BOUNDARY
  - A SOIL GROUP DESIGNATION
  - - - BOUNDARY OF INDICATED SOURCE



**SCALE REDUCED BY 1/2**

**SAN BERNARDINO COUNTY**  
HYDROLOGY MANUAL

**HYDROLOGIC SOILS GROUP MAP**  
FOR  
**SOUTHWEST-C AREA**



**SAN BERNARDINO COUNTY  
HYDROLOGY MANUAL**

REDUCED DRAWING  
SCALE 1" = 4 MILES

LEGEND:  
1.8 ISOLINES PRECIPITATION (INCHES)

**SAN BERNARDINO COUNTY  
FLOOD CONTROL DISTRICT**

**VALLEY AREA  
ISOHYETALS  
Y<sub>100</sub>-100 YEAR 1 HOUR  
BASED ON U.S.D.C. NOAA ATLAS 2, 1973**

APPROVED BY: *[Signature]*  
FLOOD CONTROL ENGINEER

DATE	SCALE	FILE NO.	DRAW. NO.
1982	1"=4M.	WRD-1	4 of 12



**NOAA Atlas 14, Volume 6, Version 2**  
**Location name: Ontario, California, USA\***  
**Latitude: 34.0548°, Longitude: -117.6835°**  
**Elevation: 938.64 ft\*\***  
 \* source: ESRI Maps  
 \*\* source: USGS



**POINT PRECIPITATION FREQUENCY ESTIMATES**

Sanja Perica, Sarah Dietz, Sarah Heim, Lillian Hiner, Kazungu Maitaria, Deborah Martin, Sandra Pavlovic, Ishani Roy, Carl Trypaluk, Dale Unruh, Fenglin Yan, Michael Yekta, Tan Zhao, Geoffrey Bonnin, Daniel Brewer, Li-Chuan Chen, Tye Parzybok, John Yarchoan

NOAA, National Weather Service, Silver Spring, Maryland

[PF\\_tabular](#) | [PF\\_graphical](#) | [Maps & aerials](#)

**PF tabular**

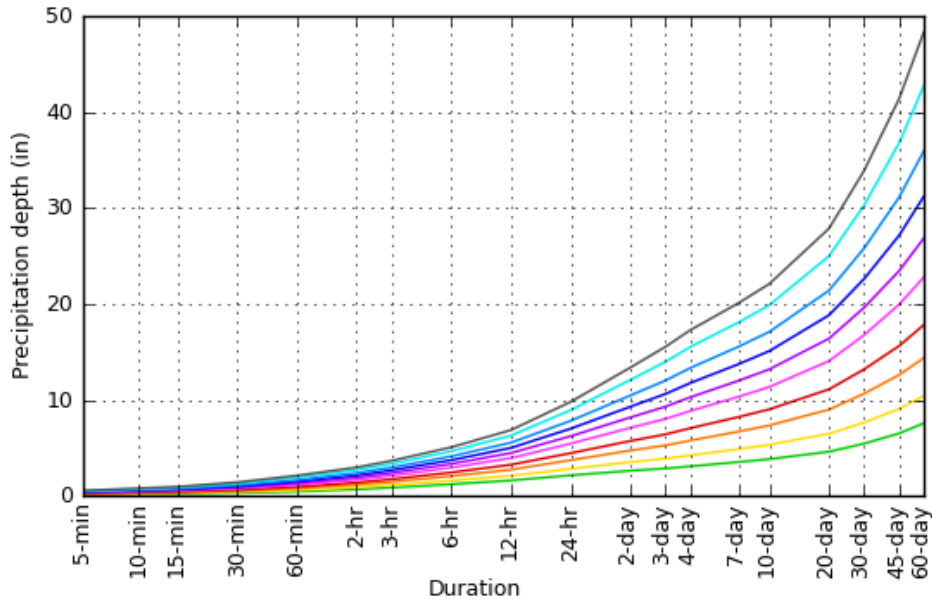
<b>PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches)<sup>1</sup></b>										
<b>Duration</b>	<b>Average recurrence interval (years)</b>									
	<b>1</b>	<b>2</b>	<b>5</b>	<b>10</b>	<b>25</b>	<b>50</b>	<b>100</b>	<b>200</b>	<b>500</b>	<b>1000</b>
<b>5-min</b>	<b>0.119</b> (0.100-0.145)	<b>0.157</b> (0.131-0.190)	<b>0.207</b> (0.172-0.251)	<b>0.248</b> (0.204-0.304)	<b>0.304</b> (0.242-0.386)	<b>0.348</b> (0.271-0.451)	<b>0.393</b> (0.298-0.523)	<b>0.440</b> (0.324-0.603)	<b>0.505</b> (0.356-0.722)	<b>0.556</b> (0.379-0.825)
<b>10-min</b>	<b>0.171</b> (0.143-0.207)	<b>0.225</b> (0.188-0.273)	<b>0.297</b> (0.246-0.360)	<b>0.355</b> (0.293-0.435)	<b>0.436</b> (0.347-0.553)	<b>0.498</b> (0.388-0.647)	<b>0.563</b> (0.427-0.749)	<b>0.630</b> (0.465-0.864)	<b>0.723</b> (0.511-1.03)	<b>0.797</b> (0.543-1.18)
<b>15-min</b>	<b>0.207</b> (0.173-0.251)	<b>0.272</b> (0.227-0.330)	<b>0.359</b> (0.298-0.436)	<b>0.429</b> (0.354-0.526)	<b>0.527</b> (0.419-0.669)	<b>0.603</b> (0.469-0.782)	<b>0.681</b> (0.517-0.906)	<b>0.762</b> (0.562-1.05)	<b>0.875</b> (0.617-1.25)	<b>0.964</b> (0.656-1.43)
<b>30-min</b>	<b>0.307</b> (0.256-0.372)	<b>0.404</b> (0.337-0.490)	<b>0.532</b> (0.442-0.646)	<b>0.637</b> (0.525-0.781)	<b>0.781</b> (0.622-0.992)	<b>0.894</b> (0.696-1.16)	<b>1.01</b> (0.766-1.34)	<b>1.13</b> (0.833-1.55)	<b>1.30</b> (0.916-1.86)	<b>1.43</b> (0.973-2.12)
<b>60-min</b>	<b>0.458</b> (0.382-0.554)	<b>0.602</b> (0.502-0.730)	<b>0.793</b> (0.659-0.964)	<b>0.950</b> (0.782-1.16)	<b>1.17</b> (0.927-1.48)	<b>1.33</b> (1.04-1.73)	<b>1.51</b> (1.14-2.00)	<b>1.69</b> (1.24-2.31)	<b>1.93</b> (1.37-2.77)	<b>2.13</b> (1.45-3.16)
<b>2-hr</b>	<b>0.689</b> (0.575-0.834)	<b>0.902</b> (0.751-1.09)	<b>1.18</b> (0.978-1.43)	<b>1.40</b> (1.15-1.72)	<b>1.70</b> (1.35-2.16)	<b>1.93</b> (1.50-2.50)	<b>2.16</b> (1.64-2.88)	<b>2.40</b> (1.77-3.29)	<b>2.73</b> (1.92-3.90)	<b>2.98</b> (2.03-4.42)
<b>3-hr</b>	<b>0.872</b> (0.728-1.06)	<b>1.14</b> (0.948-1.38)	<b>1.48</b> (1.23-1.80)	<b>1.75</b> (1.44-2.15)	<b>2.12</b> (1.69-2.69)	<b>2.40</b> (1.87-3.12)	<b>2.69</b> (2.04-3.57)	<b>2.98</b> (2.19-4.08)	<b>3.37</b> (2.38-4.82)	<b>3.67</b> (2.50-5.45)
<b>6-hr</b>	<b>1.23</b> (1.03-1.49)	<b>1.60</b> (1.33-1.94)	<b>2.07</b> (1.72-2.52)	<b>2.45</b> (2.02-3.01)	<b>2.96</b> (2.36-3.76)	<b>3.35</b> (2.61-4.34)	<b>3.74</b> (2.84-4.97)	<b>4.13</b> (3.05-5.67)	<b>4.67</b> (3.29-6.68)	<b>5.08</b> (3.46-7.54)
<b>12-hr</b>	<b>1.62</b> (1.35-1.96)	<b>2.11</b> (1.76-2.56)	<b>2.75</b> (2.28-3.34)	<b>3.26</b> (2.69-4.00)	<b>3.95</b> (3.15-5.02)	<b>4.48</b> (3.49-5.81)	<b>5.01</b> (3.81-6.68)	<b>5.56</b> (4.10-7.62)	<b>6.30</b> (4.45-9.02)	<b>6.87</b> (4.68-10.2)
<b>24-hr</b>	<b>2.16</b> (1.91-2.49)	<b>2.84</b> (2.51-3.28)	<b>3.74</b> (3.29-4.32)	<b>4.47</b> (3.91-5.21)	<b>5.47</b> (4.63-6.59)	<b>6.24</b> (5.17-7.67)	<b>7.02</b> (5.69-8.85)	<b>7.84</b> (6.17-10.2)	<b>8.95</b> (6.77-12.1)	<b>9.82</b> (7.18-13.7)
<b>2-day</b>	<b>2.64</b> (2.34-3.04)	<b>3.54</b> (3.13-4.09)	<b>4.74</b> (4.18-5.49)	<b>5.74</b> (5.02-6.69)	<b>7.11</b> (6.02-8.57)	<b>8.19</b> (6.80-10.1)	<b>9.31</b> (7.54-11.7)	<b>10.5</b> (8.26-13.6)	<b>12.1</b> (9.16-16.3)	<b>13.4</b> (9.80-18.7)
<b>3-day</b>	<b>2.87</b> (2.54-3.30)	<b>3.89</b> (3.44-4.49)	<b>5.28</b> (4.65-6.11)	<b>6.43</b> (5.62-7.50)	<b>8.04</b> (6.81-9.69)	<b>9.31</b> (7.72-11.5)	<b>10.6</b> (8.61-13.4)	<b>12.0</b> (9.48-15.6)	<b>14.0</b> (10.6-18.9)	<b>15.5</b> (11.4-21.7)
<b>4-day</b>	<b>3.09</b> (2.74-3.57)	<b>4.24</b> (3.75-4.89)	<b>5.78</b> (5.10-6.69)	<b>7.07</b> (6.18-8.24)	<b>8.87</b> (7.51-10.7)	<b>10.3</b> (8.53-12.7)	<b>11.8</b> (9.53-14.8)	<b>13.3</b> (10.5-17.3)	<b>15.5</b> (11.7-21.0)	<b>17.3</b> (12.6-24.1)
<b>7-day</b>	<b>3.54</b> (3.13-4.08)	<b>4.89</b> (4.33-5.65)	<b>6.71</b> (5.92-7.77)	<b>8.23</b> (7.20-9.60)	<b>10.3</b> (8.76-12.5)	<b>12.0</b> (9.96-14.8)	<b>13.7</b> (11.1-17.3)	<b>15.6</b> (12.3-20.1)	<b>18.1</b> (13.7-24.4)	<b>20.1</b> (14.7-28.1)
<b>10-day</b>	<b>3.84</b> (3.40-4.43)	<b>5.34</b> (4.72-6.17)	<b>7.36</b> (6.49-8.51)	<b>9.03</b> (7.90-10.5)	<b>11.4</b> (9.62-13.7)	<b>13.2</b> (10.9-16.2)	<b>15.1</b> (12.2-19.0)	<b>17.1</b> (13.5-22.1)	<b>19.9</b> (15.0-26.8)	<b>22.1</b> (16.2-30.8)
<b>20-day</b>	<b>4.62</b> (4.09-5.32)	<b>6.49</b> (5.73-7.49)	<b>9.01</b> (7.94-10.4)	<b>11.1</b> (9.72-13.0)	<b>14.1</b> (11.9-17.0)	<b>16.4</b> (13.6-20.2)	<b>18.8</b> (15.3-23.7)	<b>21.4</b> (16.9-27.7)	<b>25.0</b> (18.9-33.7)	<b>27.9</b> (20.4-38.9)
<b>30-day</b>	<b>5.45</b> (4.83-6.29)	<b>7.66</b> (6.77-8.84)	<b>10.7</b> (9.40-12.3)	<b>13.2</b> (11.5-15.4)	<b>16.8</b> (14.2-20.2)	<b>19.6</b> (16.3-24.1)	<b>22.6</b> (18.3-28.5)	<b>25.8</b> (20.3-33.4)	<b>30.3</b> (22.9-40.8)	<b>33.9</b> (24.8-47.3)
<b>45-day</b>	<b>6.52</b> (5.77-7.52)	<b>9.08</b> (8.03-10.5)	<b>12.6</b> (11.1-14.6)	<b>15.6</b> (13.7-18.2)	<b>19.9</b> (16.9-24.0)	<b>23.4</b> (19.4-28.8)	<b>27.1</b> (22.0-34.2)	<b>31.1</b> (24.5-40.3)	<b>36.8</b> (27.8-49.6)	<b>41.4</b> (30.2-57.7)
<b>60-day</b>	<b>7.57</b> (6.70-8.73)	<b>10.4</b> (9.21-12.0)	<b>14.4</b> (12.7-16.7)	<b>17.8</b> (15.6-20.8)	<b>22.8</b> (19.3-27.5)	<b>26.8</b> (22.3-33.0)	<b>31.2</b> (25.3-39.3)	<b>35.9</b> (28.3-46.5)	<b>42.7</b> (32.3-57.6)	<b>48.3</b> (35.3-67.4)

<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS). Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

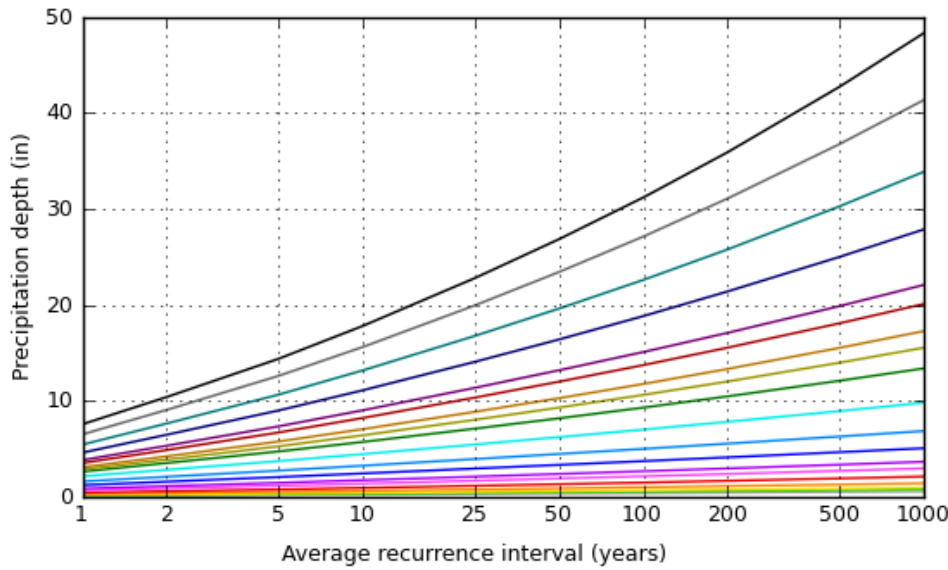
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### PF graphical

PDS-based depth-duration-frequency (DDF) curves  
Latitude: 34.0548°, Longitude: -117.6835°



Average recurrence interval (years)
1
2
5
10
25
50
100
200
500
1000

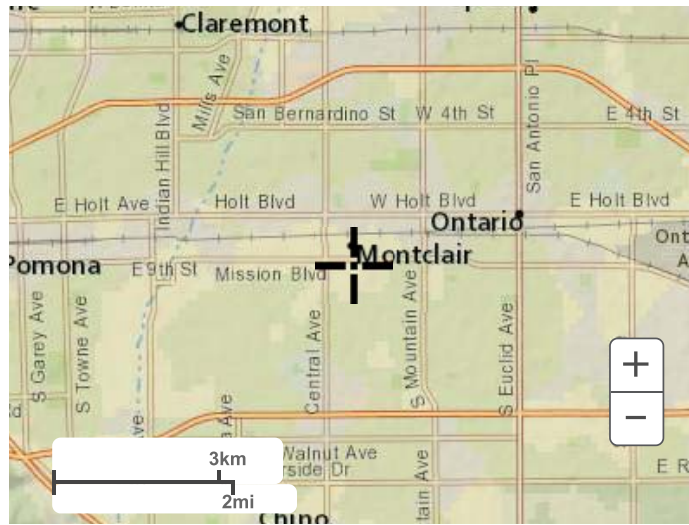


Duration
5-min
10-min
15-min
30-min
60-min
2-hr
3-hr
6-hr
12-hr
24-hr
2-day
3-day
4-day
7-day
10-day
20-day
30-day
45-day
60-day

[Back to Top](#)

### Maps & aerials

Small scale terrain



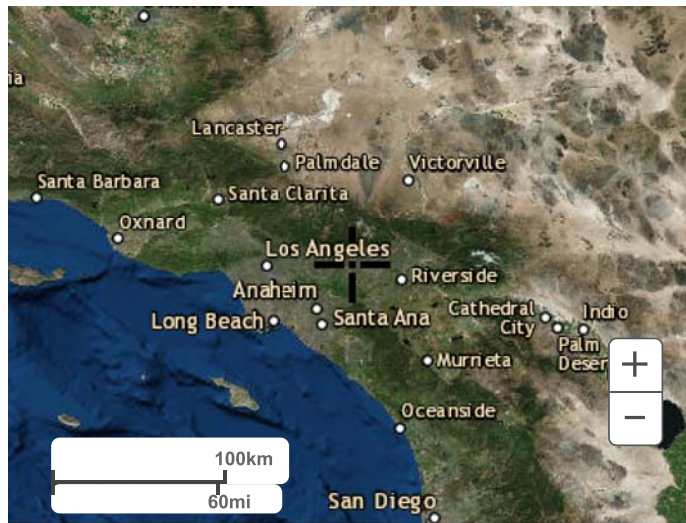
Large scale terrain



Large scale map



Large scale aerial

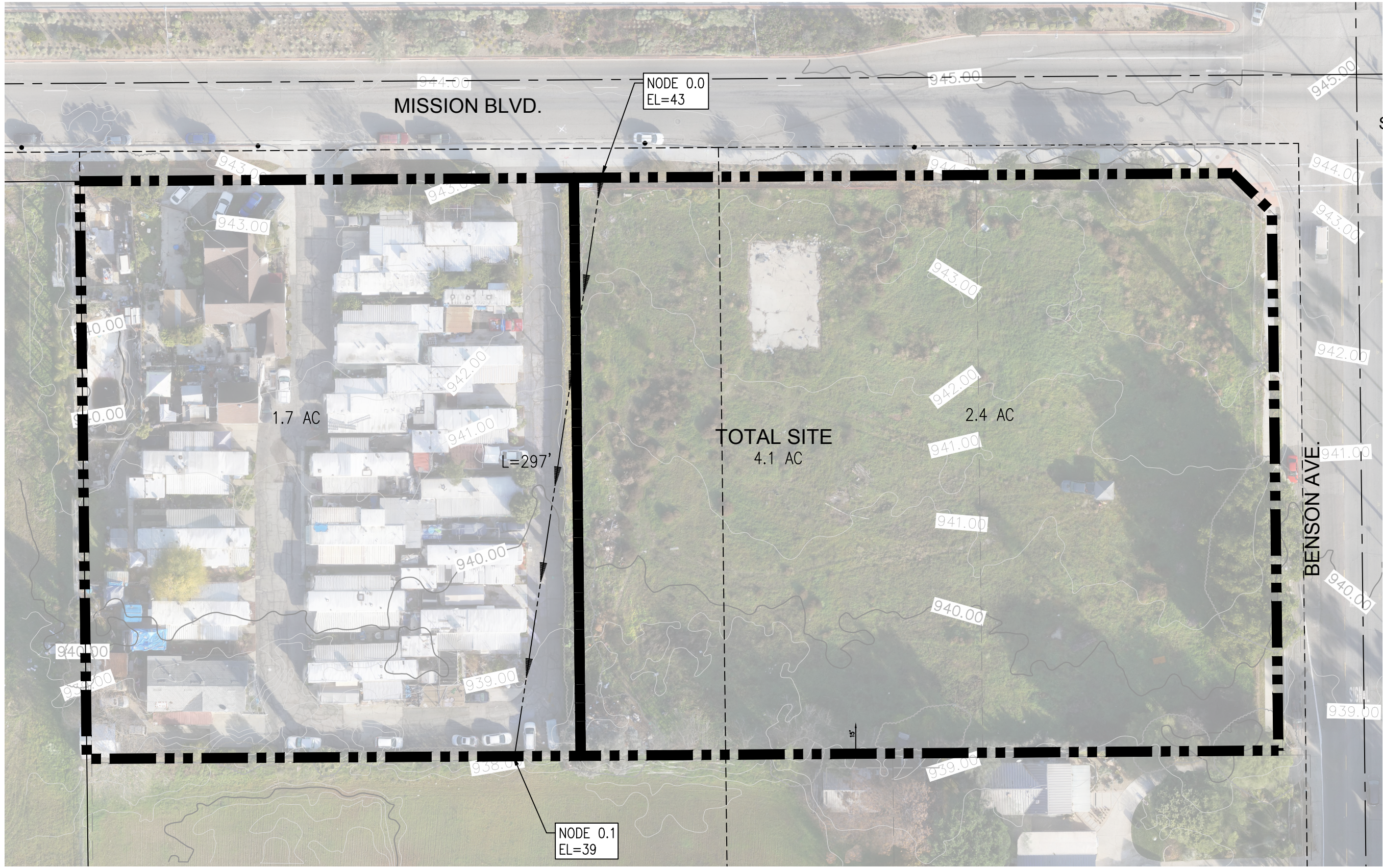


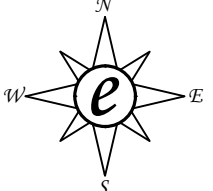
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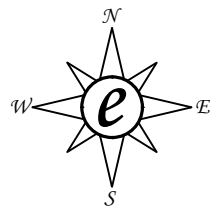
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[National Oceanic and Atmospheric Administration](#)  
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1325 East West Highway  
Silver Spring, MD 20910  
Questions?: [HDSC.Questions@noaa.gov](mailto:HDSC.Questions@noaa.gov)

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 SCALE: 1" = 50'





SCALE: 1" = 50'

